

CLAIM AMENDMENTS

Please replace the pending claims with the following listing of claims:

1. (Original) An interferometer optical switch comprising an optical waveguide circuit including:

a first optical multi/demultiplexing device;

an optical delay line including two optical waveguides connected to said first optical multi/demultiplexing device;

a second optical multi/demultiplexing device connected to said optical delay line;

one or more input waveguides connected to said first optical multi/demultiplexing device;

one or more output waveguides connected to said second optical multi/demultiplexing device; and

a phase shifter installed in said optical delay line, and wherein at least one of said first optical multi/demultiplexing device and said second optical multi/demultiplexing device is a phase generating coupler, which produces a wavelength-dependent phase difference.

2. (Original) The interferometer optical switch as claimed in claim 1, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical

multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the phase produced by the first and second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive.

3. (Original) The interferometer optical switch as claimed in claim 2, wherein the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer).

4. (Original) The interferometer optical switch as claimed in claim 2, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal throughout an entire wavelength region.

5. (Original) The interferometer optical switch as claimed in claim 2, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m'\cdot\pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

6. (Original) The interferometer optical switch as claimed in claim 1, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

7. (Original) The interferometer optical switch as claimed in claim 1, wherein said phase generating coupler is configured by connecting optical couplers and optical delay lines.

8. (Original) The interferometer optical switch as claimed in claim 7, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the phase produced by the first and second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive.

9. (Original) The interferometer optical switch as claimed in claim 8, wherein the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer).

10. (Original) The interferometer optical switch as claimed in claim 4, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of

the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal.

11. (Original) The interferometer optical switch as claimed in claim 8, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m' \cdot \pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

12. (Original) The interferometer optical switch as claimed in claim 7, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

13. (Original) The interferometer optical switch as claimed in claim 7, wherein said phase generating coupler comprises $N + 1$ optical couplers (N is a natural number), and N optical delay lines that connects adjacent optical couplers of said $N + 1$ optical couplers.

14. (Original) The interferometer optical switch as claimed in claim 13, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the phase produced by the first and second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive.

15. (Original) The interferometer optical switch as claimed in claim 14, wherein the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said

second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer).

16. (Original) The interferometer optical switch as claimed in claim 14, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal.

17. (Original) The interferometer optical switch as claimed in claim 14, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m' \cdot \pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

18. (Original) The interferometer optical switch as claimed in claim 13, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical

multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

19. (Original) The interferometer optical switch as claimed in claim 7, wherein

one of said first optical multi/demultiplexing device and said second optical multi/demultiplexing device is an optical coupler with a phase difference $2\pi\phi_c$ (constant), and the other is a phase generating coupler that is composed of two optical couplers and an optical delay line placed between said two optical couplers, and has a phase difference $2\pi\phi(\lambda)$, and wherein

assuming that ΔL is the optical path length difference of the optical delay line, and m is an integer, then the power coupling ratios of the two optical couplers constituting said phase generating coupler, and the optical path length difference of the optical delay line are set to satisfy

$$\phi(\lambda) = \Delta L/\lambda + m/2 - \phi_c \quad (11).$$

20. (Original) The interferometer optical switch as claimed in claim 19, wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta_L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta_L}(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive, and wherein

the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta_L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal throughout an entire wavelength region.

21. (Original) The interferometer optical switch as claimed in claim 19, wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive, and wherein

the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m'\cdot\pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

22. (Original) The interferometer optical switch as claimed in claim 19, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of

ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

23. (Original) The interferometer optical switch as claimed in claim 7, wherein

said first optical multi/demultiplexing device and said second optical multi/demultiplexing device are both a phase generating coupler comprising two optical couplers and a single optical delay line placed between said two optical couplers, and wherein

power coupling ratios of the two optical couplers and an optical path length difference of the optical delay line that constitutes the first and second optical multi/demultiplexing device are set such that the sum of the phase difference $2\pi\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $2\pi\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device satisfies

$$\phi_1(\lambda) + \phi_2(\lambda) = \Delta L/\lambda + m/2 \quad (12)$$

where ΔL is the optical path length difference of said optical delay line, and m is an integer.

24. (Original) The interferometer optical switch as claimed in claim 23, wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive, and wherein

the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal throughout an entire wavelength region.

25. (Original) The interferometer optical switch as claimed in claim 23, wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive,

the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m'\cdot\pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

26. (Original) The interferometer optical switch as claimed in claim 23, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference

$2\pi\{\phi_1(\lambda) + \phi_{\Delta_L}(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

27. (Previously Presented) The interferometer optical switch as claimed in claim 7, wherein

said first optical multi/demultiplexing device and said second optical multi/demultiplexing device are both a phase generating coupler comprising $N + 1$ optical couplers (N is a natural number), and N optical delay lines each of which is composed of a first and second optical waveguides, and which connects adjacent optical couplers of the $N + 1$ optical couplers, and wherein

the sum of the optical path length satisfies either $(\Sigma l_{1,1} > \Sigma l_{2,1} \text{ and } \Sigma l_{1,2} > \Sigma l_{2,2})$, or $(\Sigma l_{2,1} > \Sigma l_{1,1} \text{ and } \Sigma l_{2,2} > \Sigma l_{1,2})$, where $\Sigma l_{1,1}$ is the sum of optical path lengths of the first optical waveguide constituting the N optical delay lines of said first optical multi/demultiplexing device, $\Sigma l_{2,1}$ is the sum of optical path of the second optical waveguide, $\Sigma l_{1,2}$ is the sum of optical path lengths of the first optical waveguide constituting the N optical delay lines of said second optical multi/demultiplexing device, and $\Sigma l_{2,2}$ is the sum of optical path lengths of the second

optical waveguides constituting the N optical delay lines of said second optical multi/demultiplexing device.

28. (Original) The interferometer optical switch as claimed in claim 27, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the phase produced by the first and second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive.

29. (Original) The interferometer optical switch as claimed in claim 28, wherein the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer).

30. (Original) The interferometer optical switch as claimed in claim 28, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal.

31. (Original) The interferometer optical switch as claimed in claim 28, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m' \cdot \pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

32. (Original) The interferometer optical switch as claimed in claim 27, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity

of said optical waveguide circuit becomes uniform with respect to wavelength.

33. (Original) The interferometer optical switch as claimed in claim 27, wherein the power coupling ratios of the $N + 1$ optical couplers of said first optical multi/demultiplexing device are made equal to the power coupling ratios of the $N + 1$ optical couplers of said second optical multi/demultiplexing device.

34. (Original) The interferometer optical switch as claimed in claim 33, wherein

the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer), wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device and the optical path length

difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive, and wherein

the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal throughout an entire wavelength region.

35. (Original) The interferometer optical switch as claimed in claim 33, wherein

the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer); wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device and the optical path length

difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive, and wherein

the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m'\cdot\pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

36. (Original) The interferometer optical switch as claimed in claim 33, wherein assuming that optical wavelength is λ , a phase difference between light output from said first optical multi/demultiplexing device is $2\pi\phi_1(\lambda)$, a phase difference caused by an optical path length difference ΔL of said optical delay line is $2\pi\phi\Delta_L(\lambda)$, and a phase difference between light output from said second optical multi/demultiplexing device is $2\pi\phi_2(\lambda)$, then the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set such that output intensity of said optical waveguide circuit becomes constant for the wavelength λ .

37. (Original) The interferometer optical switch as claimed in claim 7, wherein

said first optical multi/demultiplexing device and said second optical multi/demultiplexing device each consist of a phase generating coupler including $N + 1$ optical couplers (N is a natural number), and N optical delay lines sandwiched between adjacent said optical couplers of said $N + 1$ optical couplers, and wherein

the power coupling ratios of the $N + 1$ optical couplers of said first optical multi/demultiplexing device are made equal to the power coupling ratios of the $N + 1$ optical couplers of said second optical multi/demultiplexing device.

38. (Original) The interferometer optical switch as claimed in claim 37, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the phase produced by the first and second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase

difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive.

39. (Original) The interferometer optical switch as claimed in claim 38, wherein the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer).

40. (Original) The interferometer optical switch as claimed in claim 38, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal.

41. (Original) The interferometer optical switch as claimed in claim 38, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m' \cdot \pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

42. (Original) The interferometer optical switch as claimed in claim 37, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta_L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta_L}(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

43. (Withdrawn) A variable optical attenuator that uses the interferometer optical switch as defined in claim 1 wherein, the output intensity is varied.

44. (Withdrawn) The variable optical attenuator as claimed in claim 43, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta_L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the phase produced by the first and

second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive.

45. (Withdrawn) The variable optical attenuator as claimed in claim 44, wherein the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer).

46. (Withdrawn) The variable optical attenuator as claimed in claim 44, wherein the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal throughout an entire wavelength region.

47. (Withdrawn) The variable optical attenuator as claimed in claim 44, wherein the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m' \cdot \pi$ (m' is an integer),

and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

48. (Withdrawn) The variable optical attenuator as claimed in claim 43, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

49. (Withdrawn) The variable optical attenuator as claimed in claim 43, wherein said phase generating coupler is configured by connecting optical couplers and optical delay lines.

50. (Withdrawn) The variable optical attenuator as claimed in claim 49, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical

multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the phase produced by the first and second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive.

51. (Withdrawn) The variable optical attenuator as claimed in claim 50, wherein the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer).

52. (Withdrawn) The variable optical attenuator as claimed in claim 50, wherein the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal.

53. (Withdrawn) The variable optical attenuator as claimed in claim 50, wherein the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta_L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m' \cdot \pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

54. (Withdrawn) The variable optical attenuator as claimed in claim 49, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta_L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta_L}(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

55. (Withdrawn) The variable optical attenuator as claimed in claim 49, wherein said phase generating coupler comprises $N + 1$ optical couplers (N is a natural number), and N optical delay lines that connects adjacent optical couplers of said $N + 1$ optical couplers.

56. (Withdrawn) The variable optical attenuator as claimed in claim 55, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta_L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the phase produced by the first and second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta_L}(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive.

57. (Withdrawn) The variable optical attenuator as claimed in claim 56, wherein the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer).

58. (Withdrawn) The variable optical attenuator as claimed in claim 56, wherein the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta_L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an

integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal.

59. (Withdrawn) The variable optical attenuator as claimed in claim 56, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m'\cdot\pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

60. (Withdrawn) The variable optical attenuator as claimed in claim 55, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

61. (Withdrawn) The variable optical attenuator as claimed in claim 49, wherein

one of said first optical multi/demultiplexing device and said second optical multi/demultiplexing device is an optical coupler with a phase difference $2\pi\phi_c$ (constant), and the other is a phase generating coupler that is composed of two optical couplers and an optical delay line placed between said two optical couplers, and has a phase difference $2\pi\phi(\lambda)$, and wherein

assuming that ΔL is the optical path length difference of the optical delay line, and m is an integer, then the power coupling ratios of the two optical couplers constituting said phase generating coupler, and the optical path length difference of the optical delay line are set to satisfy

$$\phi(\lambda) = \Delta L/\lambda + m/2 - \phi_c \quad (11).$$

62. (Withdrawn) The variable optical attenuator as claimed in claim 61, wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is

the phase produced by the second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive, and wherein

the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal throughout an entire wavelength region.

63. (Withdrawn) The variable optical attenuator as claimed in claim 61, wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive, and wherein

the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta_L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m'\cdot\pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

64. (Withdrawn) The variable optical attenuator as claimed in claim 61, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta_L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta_L}(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

65. (Withdrawn) The variable optical attenuator as claimed in claim 49, wherein

said first optical multi/demultiplexing device and said second optical multi/demultiplexing device are both a phase generating coupler comprising two optical couplers

and a single optical delay line placed between said two optical couplers, and wherein

power coupling ratios of the two optical couplers and an optical path length difference of the optical delay line that constitutes the first and second optical multi/demultiplexing device are set such that the sum of the phase difference $2\pi\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $2\pi\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device satisfies

$$\phi_1(\lambda) + \phi_2(\lambda) = \Delta L/\lambda + m/2 \quad (12)$$

where ΔL is the optical path length difference of said optical delay line, and m is an integer.

66. (Withdrawn) The variable optical attenuator as claimed in claim 65, wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase

difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive, and wherein

the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal throughout an entire wavelength region.

67. (Withdrawn) The variable optical attenuator as claimed in claim 65, wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive,

the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m' \cdot \pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical

multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

68. (Withdrawn) The variable optical attenuator as claimed in claim 65, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta_L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta_L}(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

69. (Withdrawn) The variable optical attenuator as claimed in claim 49, wherein

said first optical multi/demultiplexing device and said second optical multi/demultiplexing device are both a phase generating coupler comprising $N + 1$ optical couplers (N is a natural number), and N optical delay lines each of which is composed of a first and second optical waveguides,

and which connects adjacent optical couplers of the $N + 1$ optical couplers, and wherein

the sum of the optical path length satisfies either $(\Sigma l_{1,1} > \Sigma l_{2,1} \text{ and } \Sigma l_{1,2} > \Sigma l_{2,2})$, or $(\Sigma l_{2,1} > \Sigma l_{1,1} \text{ and } \Sigma l_{2,2} > \Sigma l_{1,2})$, where $\Sigma l_{1,1}$ is the sum of optical path lengths of the first optical waveguide constituting the N optical delay lines of said first optical multi/demultiplexing device, $\Sigma l_{2,1}$ is the sum of optical path lengths of the second optical waveguide, $\Sigma l_{1,2}$ is the sum of optical path lengths of the first optical waveguide constituting the N optical delay lines of said second optical multi/demultiplexing device, and $\Sigma l_{2,2}$ is the sum of optical path lengths of the second optical waveguides constituting the N optical delay lines of said second optical multi/demultiplexing device.

70. (Withdrawn) The variable optical attenuator as claimed in claim 69, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the phase produced by the first and

second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive.

71. (Withdrawn) The variable optical attenuator as claimed in claim 70, wherein the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer).

72. (Withdrawn) The variable optical attenuator as claimed in claim 70, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal.

73. (Withdrawn) The variable optical attenuator as claimed in claim 70, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m' \cdot \pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical

multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

74. (Withdrawn) The variable optical attenuator as claimed in claim 69, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

75. (Withdrawn) The variable optical attenuator as claimed in claim 69, wherein the power coupling ratios of the $N + 1$ optical couplers of said first optical multi/demultiplexing device are made equal to the power coupling ratios of the $N + 1$ optical couplers of said second optical multi/demultiplexing device.

76. (Withdrawn) The variable optical attenuator as claimed in claim 75, wherein

the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer), wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive, and wherein

the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal throughout an entire wavelength region.

77. (Withdrawn) The variable optical attenuator as claimed in claim 75, wherein

the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer); wherein

assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi_{\Delta L}(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive, and wherein

the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m'\cdot\pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

78. (Withdrawn) The variable optical attenuator as claimed in claim 75, wherein assuming that optical wavelength is

λ , a phase difference between light output from said first optical multi/demultiplexing device is $2\pi\phi_1(\lambda)$, a phase difference caused by an optical path length difference ΔL of said optical delay line is $2\pi\phi_{\Delta L}(\lambda)$, and a phase difference between light output from said second optical multi/demultiplexing device is $2\pi\phi_2(\lambda)$, then the sum $2\pi\{\phi_1(\lambda) + \phi_{\Delta L}(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set such that output intensity of said optical waveguide circuit becomes constant for the wavelength λ .

79. (Withdrawn) The variable optical attenuator as claimed in claim 49, wherein

said first optical multi/demultiplexing device and said second optical multi/demultiplexing device each consist of a phase generating coupler including $N + 1$ optical couplers (N is a natural number), and N optical delay lines sandwiched between adjacent said optical couplers of said $N + 1$ optical couplers, and wherein

the power coupling ratios of the $N + 1$ optical couplers of said first optical multi/demultiplexing device are made equal to the power coupling ratios of the $N + 1$ optical couplers of said second optical multi/demultiplexing device.

80. (Withdrawn) The variable optical attenuator as claimed in claim 79, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the phase produced by the first and second optical multi/demultiplexing device and the optical path length difference ΔL is set such that the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ becomes wavelength insensitive.

81. (Withdrawn) The variable optical attenuator as claimed in claim 80, wherein the sum of the phase difference $\phi_1(\lambda)$ of the output of said first optical multi/demultiplexing device and the phase difference $\phi_2(\lambda)$ of the output of said second optical multi/demultiplexing device equals $\Delta L/\lambda + m/2$ (m is an integer).

82. (Withdrawn) The variable optical attenuator as claimed in claim 80, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $(2m' + 1) \cdot \pi$ (m' is an

integer), and the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device are made equal.

83. (Withdrawn) The variable optical attenuator as claimed in claim 80, wherein the sum $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ of the three phase differences is set at $2m'\cdot\pi$ (m' is an integer), and the sum of the power coupling ratio of said first optical multi/demultiplexing device and the power coupling ratio of said second optical multi/demultiplexing device is made unity.

84. (Withdrawn) The variable optical attenuator as claimed in claim 79, wherein assuming that λ is the wavelength, $2\pi\phi_1(\lambda)$ is the phase produced by the first optical multi/demultiplexing device, $2\pi\phi\Delta_L(\lambda)$ is the phase difference of the optical delay line with an optical path length difference of ΔL , and $2\pi\phi_2(\lambda)$ is the phase produced by the second optical multi/demultiplexing device, the sum of the phase difference $2\pi\{\phi_1(\lambda) + \phi\Delta_L(\lambda) + \phi_2(\lambda)\}$ is set such that the output intensity of said optical waveguide circuit becomes uniform with respect to wavelength.

85. (Previously Presented) An interferometer optical switch comprising a plurality of interferometer optical switches as defined in claim 1 connected in cascade.

86. (Withdrawn) A variable optical attenuator comprising a plurality of variable optical attenuators as defined in claim 43 connected in cascade.

87. (Previously Presented) An interferometer optical switch comprising an optical circuit having a plurality of interferometer optical switches as defined in claim 1 connected in cascade, wherein

a first interferometer optical switch having two output waveguides;

one of the said output waveguides is connected to the input waveguide of a second interferometer optical switch;

the other output waveguide of said first interferometer optical switch is used as the second output port of said optical circuit;

the input waveguide of said first interferometer optical switch is used as the input port of said optical circuit; and

the output waveguide of said second interferometer optical switch is used as the first output port of said optical circuit.

88. (Withdrawn) A variable optical attenuator comprising an optical circuit having a plurality of variable optical attenuators as defined in claim 43 connected in cascade, wherein

a first interferometer optical switch having two output waveguides;

one of the said output waveguides is connected to the input waveguide of a second interferometer optical switch;

the other output waveguide of said first interferometer optical switch is used as the second output port of said optical circuit;

the input waveguide of said first interferometer optical switch is used as the input port of said optical circuit; and

the output waveguide of said second interferometer optical switch is used as the first output port of said optical circuit.

89. (Previously Presented) An interferometer optical switch comprising an optical circuit having a plurality of

interferometer optical switches as defined in claim 1 connected in cascade, wherein

a first interferometer optical switch having two output waveguides;

one of the said output waveguides is connected to the input waveguide of a second interferometer optical switch;

the other output waveguide of said first interferometer optical switch is connected to the input waveguide of a third interferometer optical switch;

the input waveguide of said first interferometer optical switch is used as the input port of said optical circuit;

the output waveguide of said second interferometer optical switch is used as the first output port of said optical circuit; and

the output waveguide of said third interferometer optical switch is used as the second output port of said optical circuit.

90. (Withdrawn) A variable optical attenuator comprising an optical circuit having a plurality of optical variable attenuates as defined in claim 43 connected in cascade, wherein

a first interferometer optical switch having two output waveguides;

one of the said output waveguides is connected to the input waveguide of a second interferometer optical switch;

the other output waveguide of said first interferometer optical switch is connected to the input waveguide of a third interferometer optical switch;

the input waveguide of said first interferometer optical switch is used as the input port of said optical circuit;

the output waveguide of said second interferometer optical switch is used as the first output port of said optical circuit; and

the output waveguide of said third interferometer optical switch is used as the second output port of said optical circuit.

91. (Previously Presented) An interferometer optical switch using at least one interferometer optical switch as defined in claim 1 to configure an optical switch with M inputs (M: natural number) and N outputs (N: natural number).

92. (Withdrawn) A variable optical attenuator using at least one variable optical attenuator as defined in claim 43 to configure an optical switch with M inputs (M: natural number) and N outputs (N: natural number).

93. (Previously Presented) The interferometer optical switch as claimed in claim 1, wherein said optical coupler consists of a directional coupler including two optical waveguides placed side by side in close proximity.

94. (Withdrawn) The variable optical attenuator as claimed in any one of claims claim 43, wherein said optical coupler consists of a directional coupler including two optical waveguides placed side by side in close proximity.

95. (Previously Presented) The interferometer optical switch as claimed in claim 1, wherein said phase shifter consists of a thin film heater formed on the optical waveguide.

96. (Withdrawn) The variable optical attenuator as claimed in claim 43, wherein said phase shifter consists of a thin film heater formed on the optical waveguide.

97. (Currently Amended) The interferometer optical switch as claimed in claim 1, wherein said phase shifter consists of a thin film heater formed ~~on the optical waveguide, and~~ near an adiabatic groove ~~is formed near said thin film heater~~ on the optical waveguide.

98. (Withdrawn) The variable optical attenuator as claimed in claim 43, wherein said phase shifter consists of a thin film heater formed on the optical waveguide, and an adiabatic groove is formed near said thin film heater.

99. (Previously Presented) The interferometer optical switch as claimed in claim 1, wherein said optical waveguide circuit is made of a silica-based glass optical waveguide.

100. (Withdrawn) The variable optical attenuator as claimed in claim 43, wherein said optical waveguide circuit is made of a silica-based glass optical waveguide.

101. (Currently Amended) The interferometer optical switch as claimed in claim 1, wherein said interferometer optical switch ~~has birefringent index adjustment means on its optical waveguide, or~~ undergoes adjustment of a birefringent index.

102. (Withdrawn) The variable optical attenuator as claimed in claim 43, wherein said variable optical attenuator has birefringent index adjustment means on its optical waveguide, or undergoes adjustment of a birefringent index.

103. (Previously Presented) An optical module comprising a module including within it an interferometer optical switch as defined in claim 1, and optical fibers that are held by said module for inputting and outputting a signal to and from said interferometer optical switch.

104. (Withdrawn) An optical module comprising a module including within it a variable optical attenuator as defined in claim 43, and optical fibers that are held by said module for inputting and outputting a signal to and from said variable attenuator.